

How to Specify Durable and Sustainable Concrete

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Concrete





Cernent Water Air Fine address Coarse address 25% C

Outline



- Specifying the correct exposure class
- Specification methods
- Aggregates
- Cements and combinations
- Use of admixtures
- Responsible sourcing
- Further information



Intended Working Life



BS EN 1990: 2002 'Eurocode - Basis of structural design'

Temporary structures	10 years
Replaceable structural parts	10-25 years
Agricultural and similar structures	15-30 years
Building structures and other common structures	50 years
Monumental buildings; Bridges; Civil engineering structures	100 years

Intended Working Life



Table A.4	Durability recommendations for reinforced or prestressed elements with an intended working life of at	
	leas 50 years	

Nominal cover ¹³⁾		Compressive strength class where recommended, maximum water-cement ratio and minimum cement or combination content for normal-weight concrete $^{\rm C}$ with 20 mm maximum aggregate size $^{\rm D}$)										
mm	$15 + \Delta c$	$20 + \Delta c$	$25 + \Delta c$	$30 + \Delta c$	$35 + \Delta c$	$40 + \Delta c$	$45 + \Delta c$	$50 + \Delta c$				
Corrosio	n induced by	carbonation (XC exposure cl	asses)								
XC1	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	All in Table A.6			
XC2			C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	All in Table A.6			
vesu	-	C40/50 0.45 340	C30/37 0,55 300	C28/35 0,60 280	C25/30 0.65 260	C25/30 0.65 260	C25/30 0,65 260	C25/30 0.65 260	All in Table A.6 except IVB-V			
XC3/4	-	_	C40/50 0.45 340	C30/37 0.55 300	C28/35 0.60 280	C25/30 0.65 260	C25/30 0,65 260	C25/30 0.65 260	IVB-V			
				r, XD other than d corrosion (XC)								
XD1	-	1,=	C40/50 0.45 360	C32/40 0.55 320	C28/35 0.60 300	C28/35 0.60 300	C28/35 0.60 300	C28/35 0.60 300	All in Table A.6			
	-		-	C45/55 ^{E)} 0,35 ^{F)} 380	C35/45 ^{E)} 0.45 360	C32/40 ^{E)} 0.50 340	C32/40 ^{E)} 0.50 340	C32/40 ^{E)} 0.50 340	CEM I, IIA, IIB-S, SRPC			
vo.	-	-	_	C40/50 ^{E)} 0.35 ^{F)} 380	C32/40 ^{E)} 0.45 360	C28/35 0.50 340	C25/30 0.55 320	C25/30 0.55 320	ІІВ-У, ША			
XS1	-	-	-	C32/40 ^{E)} 0.40 380	C25/30 0.50 340	C25/30 0.50 340	C25/30 0.55 320	C25/30 0.55 320	шв			
	-	-	-	C32/40 ^{E)} 0.40 380	C28/35 0.50 340	C25/30 0.50 340	C25/30 0.55 320	C25/30 0.55 320	IVB-V			
			-	C40/50 ⁽⁵⁾ 0.40 380	C32/40 ^{E)} 0.50 340	C28/35 0.55 320	C28/35 0.55 320	C28/35 0.55 320	CEM I, IIA, IIB-S, SRPC			
XD2 or XS2	-	(<u>3)</u>	_	C35/45 ^{E)} 0.40 380	C28/35 0.50 340	C25/30 0.55 320	C25/30 0.55-320	C25/30 0.55 320	пв-у, ша			
	-	-	-	C32/40 ^(c) 0.40 380	C25/30 0.50 340	C20/25 0.55 320	C20/25 0.55 320	C20/25 0.55 320	IIIB, IVB-V			

Intended Working Life



Table A.5	Durability - recommendations for reinforced or prestressed elements with an intended working life	of at
	least 100 years	

cover ^{B)}		Compressive strength class where recommended, maximum water-cement ratio and minimum cement or combination content for normal-weight concrete ⁽²⁾ with 20 mm maximum aggregate size ⁽³⁾									
mm	15 + Δc	$25 + \Delta c$	$30 + \Delta c$	$35 + \Delta c$	$40 + \Delta c$	$45 + \Delta c$	$50 + \Delta c$	$55 + \Delta e$	$60 + \Delta c$	65 + ∆c	
Corrosio	n induced	by carbonat	ion (XC exp	osure classe	s)						
XC1	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	C20/25 0.70 240	All in Table A.6
C2		C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	All in Table A.6
	-	-	C40/50 0.45 340	C35/45 0.50 320	C30/37 0.55 300	C28/35 0.60 280	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	C25/30 0.65 260	All in Table A.6 except IVB-V
C3/4	-	_	1-	C40/50 0,45 340	C35/45 0.50 320	C30/37 0,55 300	C28/35 0.60 280	C25/30 0.65 260	C25/30 0.65 260	C25/30 0,65 260	IVB-V
			(XS from set carbonation		other than	sea water)		- Handada			
XD1	-	<u></u>	C45/55 0.40 380	C40/50 0.45 360	C35/45 0.50 340	C32/40 0.55 320	C28/35 0.60 300	C28/35 0.60 300	C28/35 0.60 300	C28/35 0.60 300	All in Table A.6
		-	- Contraction	-	- 10 1	C45/55 ^{E)} 0,35 ^{F)} 380	C40/50 ^{E)} 0.40 380	C35/45 ⁽⁵⁾ 0.45 360	C35/45 ^{E)} 0.45 360	C35/45 ^(B) 0.45 360	CEM I, IIA, IIB-S, SRPC
761		-	_	C35/45 0.40 380	C32/40 ^{E)} 0.45 360	C28/35 0.50 340	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	IIB-V, IIIA
(SI	-	-	-	C35/45 0.45 360	C30/37E) 0.50 340	C28/35 0.55 320	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	шв
	-	-	-	C40/50 0.45 360	C35/45 0.50 340	C30/37 0,55 320	C28/35 0.55 320	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	IVB-V
	-	-	-	-	C35/45 ^{E)} 0.45 360	C32/40 ^{E)} 0.50 340	C28/35 0.55 320	C28/35 0.55 320	C28/35 0.55 320	C28/35 0.55 320	CEM I, IIA, IIB-S, SRPC
XD2 or XS2	-	-	-	-	C32/40 [©] 0.45 360	C28/35 0.50 340	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	C25/30 0.55 320	IIB-V, IIIA
				77	C28/35	C25/30	C20/25	C20/25	C20/25	C20/25	IIIB, IVB-V



XC: Corrosion induced by carbonation

XD: Corrosion induced by chlorides

XS: Corrosion induced by chlorides from sea

XF: Freeze-thaw attack





XC: Corrosion induced by carbonation



XD: Corrosion induced by chlorides



XS: Corrosion induced by chlorides from sea

XF: Freeze-thaw attack



XC: Corrosion induced by carbonation

XC1: Dry or permanently wet

XC2: Wet, rarely dry

XC3: Moderate humidity

XC4: Cyclic wet and dry

XD: Corrosion induced by chlorides

XS: Corrosion induced by chlorides from sea

XF: Freeze-thaw attack





XC: Corrosion induced by carbonation

XD: Corrosion induced by chlorides

XD1: Moderate humidity

XD2: Wet, rarely dry

XD3: Cyclic wet and dry

XS: Corrosion induced by chlorides from sea

XF: Freeze-thaw attack





XC: Corrosion induced by carbonation

Corrosion induced by chlorides

XS: Corrosion induced by chlorides from sea

XS1: Exposed to airborne salt

XS2: Permanently submerged

XS3: Tidal, splash and spray zones

XF: Freeze-thaw attack

XD:



XC: Corrosion induced by carbonation

XD: Corrosion induced by chlorides

XS: Corrosion induced by chlorides from sea

XF: Freeze-thaw attack

AC: Chemical attack

XF1: Moderate water saturation (no de-icing agent)

XF2: Moderate water saturation (de-icing agent)

XF3: High water saturation, (no de-icing agent)

XF4: High water saturation (de-icing agent)



XC: Corrosion induced by carbonation

XD: Corrosion induced by chlorides

XS: Corrosion induced by chlorides from sea

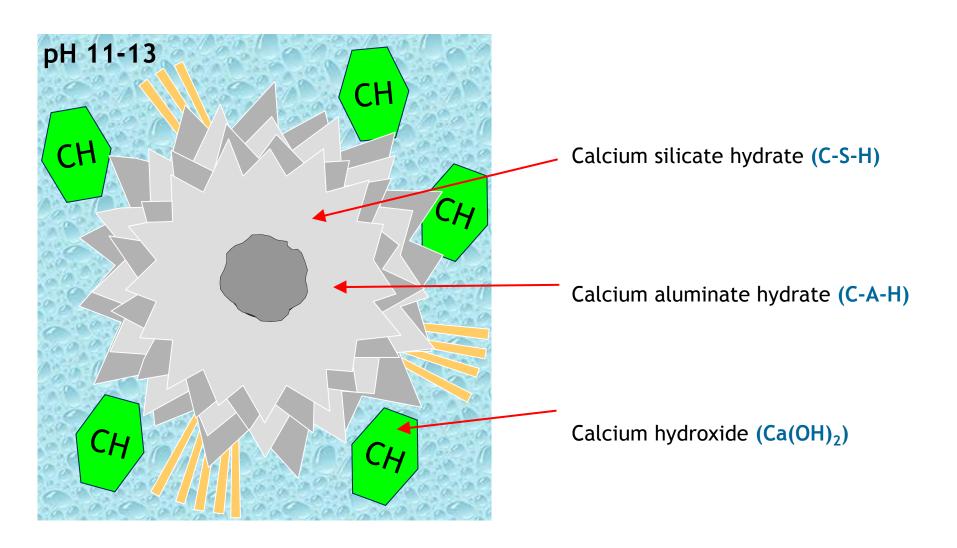
XF: Freeze-thaw attack





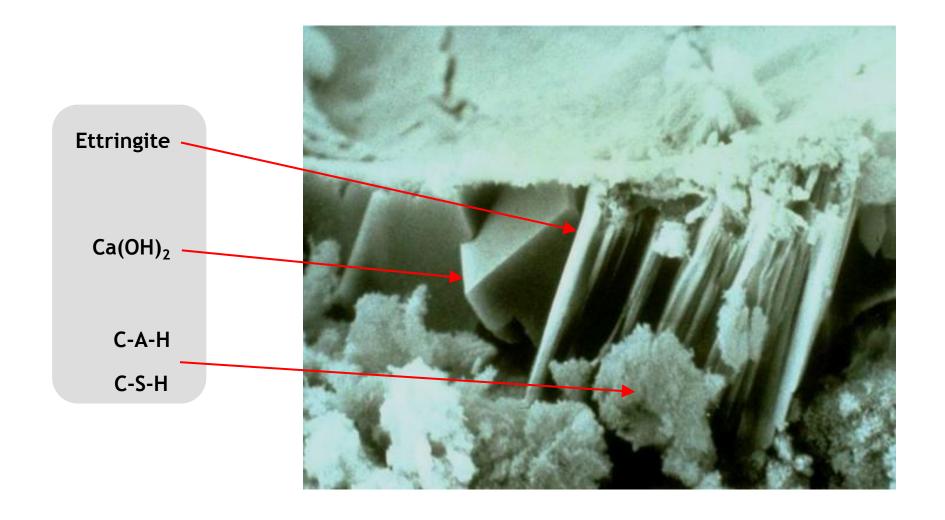
Cement Hydration





Cement Hydration



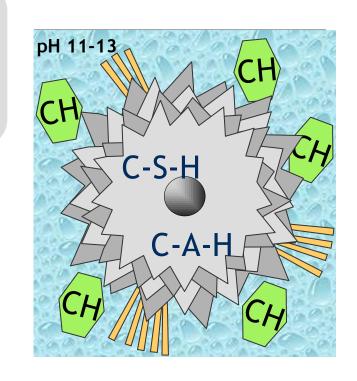


Conventional Sulfate Attack



Sulfate + C-A-H =
$$3\text{CaO.Al}_2\text{O}_3.3\text{CaSO}_4.31\text{H}_2\text{O}$$
 (ettringite)

Sulfate +
$$Ca(OH)_2$$
 = $CaSO_4.2H_2O$
(gypsum)



Result is expanison

Conventional Sulfate Attack



Sulfate + C-A-H =
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(gypsum)



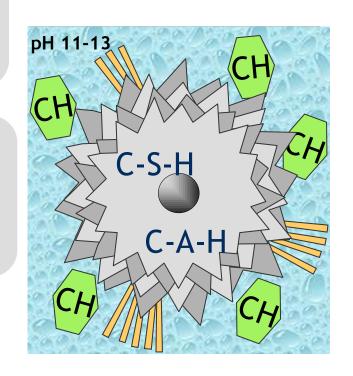
Result is expansion

Thaumasite form of Sulfate Attack ((mpa



 CO_3 / low temperature (<15°) / high pH (\geq 10.5)

Sulfates + C-S-H = $CaSiO_3.CaCO_3.$ $CaSO_4.15H_2O$ (thaumasite)



Result is weakening and some expansion

Thaumasite form of Sulfate Attack ((mpa



 CO_3 / low temperature (<15°) / high pH (\geq 10.5)

Sulfates + C-S-H = CaSiO₃.CaCO₃.

CaSO₄.15H₂O

(thaumasite)



Result is weakening and some expansion

DS and ACEC Classes - Natural Ground



Sulfate				Groundwat	er	ACEC
Design Sulfate Class for location	2:1 water/soil extract ^b	Groundwater	Total potential sulfate ^c	Static water	Mobile water	Class for location
1	2 (SO ₄ mg/l)	3 (SO ₄ mg/I)	4 (SO ₄ %)	5 (pH)	6 (pH)	7
DS-1	< 500	< 400	< 0.24	≥2.5		AC-1s
					> 5.5 ^d	AC-1 ^d
					2.5-5.5	AC-2z
DS-2	500-1500	400–1400	0.24-0.6	> 3.5		AC-1s
			N C TO SELECTION		> 5.5	AC-2
				2.5-3.5		AC-2s
					2.5-5.5	AC-3z
DS-3	1600-3000	1500-3000	0.7-1.2	> 3.5		AC-2s
					> 5.5	AC-3
				2.5-3.5		AC-3s
					2.5-5.5	AC-4
DS-4	3100–6000	3100-6000	1.3-2.4	> 3.5		AC-3s
					> 5.5	AC-4
				2.5-3.5		AC-4s
					2.5-5.5	AC-5
DS-5	> 6000	> 6000	> 2.4	> 3.5		AC-4s
				2.5-3.5	≥ 2.5	AC-5

DS and ACEC Classes - Natural Ground



Sulfate				Groundwat	er	ACEC
Design Sulfate Class for location	2:1 water/soil extract b	Groundwater	Total potential sulfate ^c	Static water	Mobile water	Class for location
1	2 (SO ₄ mg/I)	3 (SO ₄ mg/I)	4 (SO ₄ %)	5 (pH)	6 (pH)	7
DS-1	< 500	< 400	< 0.24	≥2.5		AC-1s
					> 5.5 ^d	AC-1 ^d
					2.5-5.5	AC-2z
DS-2	500-1500	400-1400	0.24-0.6	> 3.5		AC-1s
					> 5.5	AC-2
				2.5-3.5	S*:	AC-2s
					2.5-5.5	AC-3z
DS-3	1600-3000	1500-3000	0.7-1.2	> 3.5		AC-2s
					> 5.5	AC-3
				2.5-3.5		AC-3s
					2.5-5.5	AC-4
DS-4	3100-6000	3100-6000	1.3-2.4	> 3.5		AC-3s
					> 5.5	AC-4
				2.5-3.5		AC-4s
					2.5-5.5	AC-5
DS-5	> 6000	> 6000	> 2.4	> 3.5		AC-4s
				2.5-3.5	≥ 2.5	AC-5

DC Class and APMs



ACEC Class	Intended working life						
(from Tables C1 and C2)	At least 50 years ^{d,e}	At least 100 years					
AC-1s, AC-1	DC-1	DC-1					
AC-2s, AC-2	DC-2	DC-2					
AC-2z	DC-2z	DC-2z					
AC-3s	DC-3	DC-3					
AC-3z	DC-3z	DC-3z					
AC-3	DC-3	DC-3 + one APM of choice					
AC-4s	DC-4	DC-4					
AC-4z	DC-4z	DC-4z					
AC-4	DC-4	DC-4 + one APM of choice					
AC-4ms	DC-4m	DC-4m					
AC-4m	DC-4m	DC-4m + one APM of choice					
AC-5z	DC-4z + APM3f	DC 4z + APM3 ^t					
AC-5	DC-4 + APM3 ^f	DC-4 + APM3 ^f					
AC-5m	DC-4m + APM3 ^f	DC-4m + APM31					

Specification Method



Designated concrete

Designed concrete

Prescribed concrete

Standardised prescribed concrete

Proprietary concrete

BS 8500-1:2002 BRITISH STANDARD Concrete — Complementary British Standard to BS EN 206-1 — Part 1: Method of specifying and guidance for the specifier 108 91 100 38 NO COPYING WITHOUT BRE PERMISSION EXCEPT AS PERMITTED BY COPYRIGHT LAW



- Simple and reliable form of specification, widely used
- Strength, durability performance requirements specified
- Maximum aggregate size and consistency specified

 Producer can vary cement and combination types, aggregates etc.

Cannot be used in presence of chlorides



Basic specification requirements

- Concrete designation
- Max. aggregate size
- Consistence class

Other?





Basic specification requirements

- Concrete designation
- Max. aggregate size
- Consistence class

Other?

- Restriction / relaxation of cement type
- Special aggregate requirements
- Accelerated / retarded set
- Colour
- Fibres / air content





BS 8500-1: 2006 (Table A.3)

Use	Exposure class	Nominal cover A)	Minimum designated
		mm	concrete B)
Reinforced and prestressed concrete inside enclosed buildings except poorly ventilated rooms with high humidity	XC1	$(15 + \Delta c)$	RC20/25
		$(20 + \Delta c)$	RC40/50
External reinforced and prestressed vertical elements of buildings sheltered from, or exposed to, rain ^{C)}	XC3/XC4 + XF1	$(25 + \Delta c)$	RC32/40
ballangs shellered from, or exposed to, run		$(30 + \Delta c)$	RC28/35
		$(20 + \Delta c)$	RC40/50XF
Horizontal elements with high saturation without de-icing agent and subject to freezing while wet ^{C)}	XC4+XF3	$(30 + \Delta c)$	PAV2
agent and subject to freezing wine wet		$(35 + \Delta c)$	PAV1
Reinforced or prestressed buried foundation in AC-1 where the hydraulic gradient is not greater than 5	XC2/AC-1	50 D) 75 E)	RC25/30
C25/30 reinforced or prestressed buried foundation in AC-2 or more aggressive ground conditions	AC-2 to AC-5m	50 D) 75 E)	See F)



BS 8500-2: 2006 (Table 5)

Concrete designation	Min. strength class	Slump class ^{A)}	Max. w/c ratio	Min. cement or combination content (kg/m³) for max. aggregate size (mm)				Cement and combination types
				≽40	20	14	10	_
GEN0	C6/8	S3	·—	120	120	120	120	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
GEN1	C8/10	S3	_	180	180	180	180	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
GEN2	C12/15	S3	_	200	200	200	200	${\rm CEM\ I,\ IIA,\ IIB\text{-}S,\ IIB\text{-}V,\ IIIA,\ IVB\text{-}V}$
GEN3	C16/20	S3	_	220	220	220	220	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
RC20/25	C20/25	S3	0.70	240	240	260	280	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
RC25/30	C25/30	S3	0.65	240	260	280	300	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC28/35	C28/35	S3	0.60	260	280	300	320	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC30/37	C30/37	S3	0.55	280	300	320	340	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V B)
RC32/40	C32/40	S3	0.55	280	300	320	340	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC35/45	C35/45	S3	0.50	300	320	340	360	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC40/50	C40/50	S3	0.45	320	340	360	360	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$



BS 8500-1: 2006 (Table A.3)

Use	Exposure class	Nominal cover A)	Minimum
		mm	designated concrete B)
Reinforced and prestressed concrete inside enclosed buildings except poorly ventilated rooms with high humidity	XC1	$(15 + \Delta c)$	RC20/25
		$(20 + \Delta c)$	RC40/50
External reinforced and prestressed vertical elements of buildings sheltered from, or exposed to, rain ^{C)}	XC3/XC4 + XF1	$(25 + \Delta c)$	RC32/40
		$\frac{(30 + \Delta c)}{(20 + \Delta c)}$	RC28/35 RC40/50XF
Horizontal elements with high saturation without de-icing agent and subject to freezing while wet $^{\rm C)}$	XC4+XF3	$(30 + \Delta c)$	PAV2
		$(35 + \Delta c)$	PAV1
Reinforced or prestressed buried foundation in AC-1 where the hydraulic gradient is not greater than 5	XC2/AC-1	50 D) 75 E)	RC25/30
C25/30 reinforced or prestressed buried foundation in AC-2 or more aggressive ground conditions	AC-2 to AC-5m	50 ^{D)} 75 ^{E)}	See ^{F)}

Specification



BS 8500-2: 2006 (Table 5)

Concrete designation	Min. strength class	Slump class ^{A)}	Max. w/c ratio	Min. cement or combination content (kg/m³) for max. aggregate size (mm)				Cement and combination types
				≽40	20	14	10	_
GEN0	C6/8	S3	·—	120	120	120	120	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
GEN1	C8/10	S3	5 1	180	180	180	180	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
GEN2	C12/15	S3	_	200	200	200	200	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
GEN3	C16/20	S3	_	220	220	220	220	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
RC20/25	C20/25	S3	0.70	240	240	260	280	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V
RC25/30	C25/30	S3	0.65	240	260	280	300	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC28/35	C28/35	S3	0.60	260	280	300	320	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC30/37	C30/37	S3	0.55	280	300	320	340	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC32/40	C32/40	S3	0.55	280	300	320	340	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC35/45	C35/45	S3	0.50	300	320	340	360	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$
RC40/50	C40/50	S3	0.45	320	340	360	360	CEM I, IIA, IIB-S, IIB-V, IIIA, IVB-V $^{\mathrm{B})}$



- Permit flexibility
- Suitable for most applications
- Strength, allowable cement types; water/cement ratios; use of recycled or secondary aggregates are specified

- Appropriate for concrete with focus on eCO₂
- To be used for specification of visual cast insitu concrete



Basic specification requirements

- Strength class
- Max. W/C ratio
- Cement type and min. content
- Max. aggregate size
- Consistence class
- Chloride class
- Density class



Other?



Additional specification options

- •Aggregate type, including use of recycled aggregate
- Fibres if used
- Air entrainment
- •Temperature of the fresh concrete
- •Heat development during hydration
- Resistance to water penetration
- Tensile strength
- Resistance to abrasion



Prescribed Concretes



- Exact composition of concrete specified
- Specifier takes full design responsibility including testing



Standardised Prescribed Concretes



- Small construction sites, with small scale batching.
- Strength is not of critical importance







- Developed by concrete producer as a proprietary product
- Composition not disclosed.
- Specified performance requirements confirmed
- Low eCO₂ concretes available
- Used for pre-cast concrete specifications



Aggregates





- Major component of concrete by volume
- Inherently low carbon
- Mostly naturally occurring, local resource
- Also recycled aggregate (RA) recycled concrete aggregate (RCA) and secondary aggregates
- 28% of all aggregate in UK is recycled or secondary aggregate (highest in Europe)



Recycled Aggregates: Types

 Recycled aggregate (RA)- Resulting from reprocessing of inorganic material previously used in construction

 Recycled concrete aggregate (RCA) - RA principally comprising crushed concrete

 Secondary aggregates - Arising from other processes eg: blast furnace and zinc slag; foundry sand; slate aggregate; china clay sand or stent

Recycled aggregates



Table 1: Use of RA and RCA in BS 8500 for
Designated Concrete

Designated concrete	Percentage of coarse aggregate in RA or RCA
GEN 0 to GEN 3	100%
RC20/25 to RC40/50	20%*
RC40/50XF	0%
PAV1 & PAV2	0%
FND2 to FND4	0%



•Local virgin aggregates will have lower eCO₂ than RA transported longer distances (over 15km by road)







- Recycled Aggregates are efficiently used as hardcore and in landscaping
- Very little (effectively none) goes into landfill
- Consistency of supply and source material are necessary for use in concrete
- Testing regimes for quality control is more rigorous than for natural/primary aggregates

Secondary aggregates



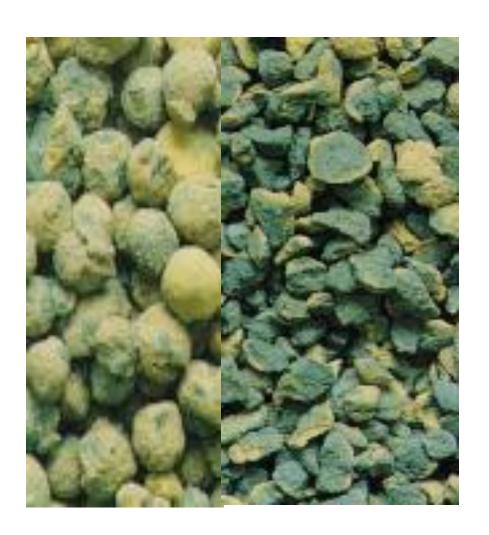


Granite sand/aggregate(formerly known as stent)

 Waste granite rock material that has been separated from Kaolin (china clay) by high pressure water jets.

Secondary aggregates





Lytag:

- Sintered pulverised fuel ash lightweight aggregate
- Weight of structural concrete reduced by 25%

Primary aggregates

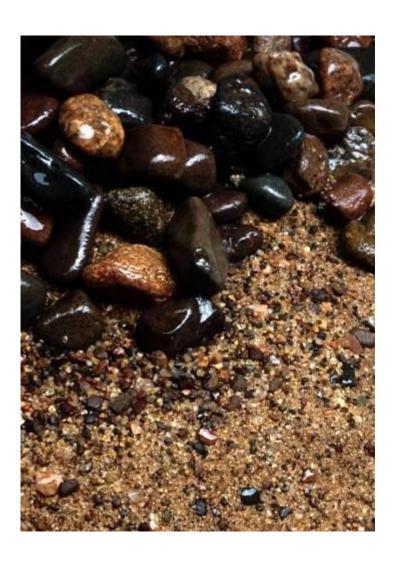




- Predominantly UK sourced
- Reserves in UK will last for hundreds of thousands of years
- Tightly regulated extraction for environmental impacts
- Life cycle of a quarry is environmentally positive
- Over 700 areas of Special Scientific Interest are former mineral extraction sites

Aggregate and cement content





- Size of aggregate impacts on cement content
- Smaller aggregate requires a higher cement content
- Some RA and RCA require higher cement content to achieve strength

Specification tips



- Permit recycled and secondary aggregate but do not over specify
- Consider locally available natural sources to reduce ECO2
- Do not specify aggregate sizes below 10mm unless necessary
- If available and appropriate specify recycled or secondary aggregates in footings

Cement Specification

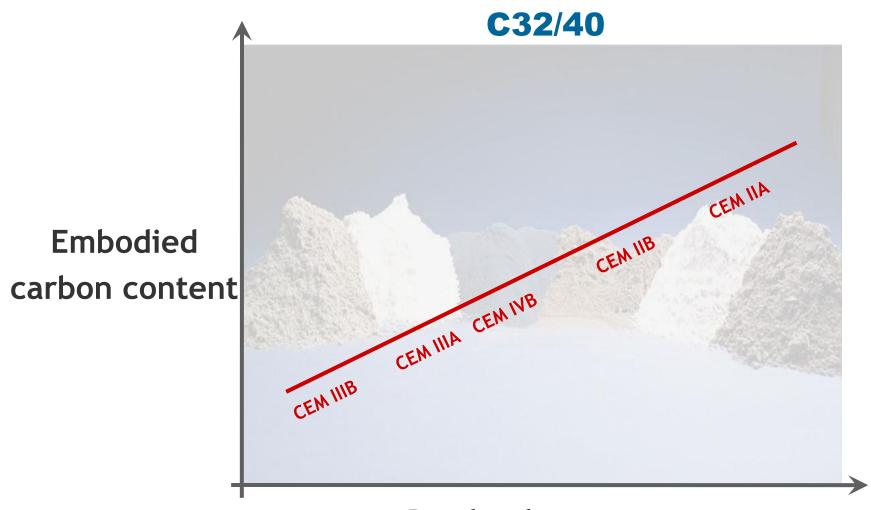




Туре	Addition	Portland cement replacement, %	
CEM I	~	0 – 5	
IIA	Silica fume	6 – 10	
IIA	Fly ash	6 – 20	
IIB-V	The sole	21 – 35	
IVB-V	Fly ash	36 – 55	
IIB-S		21 – 35	
IIIA	GGBS	36 – 65	
IIIB		66 – 80	

Cements and combinations

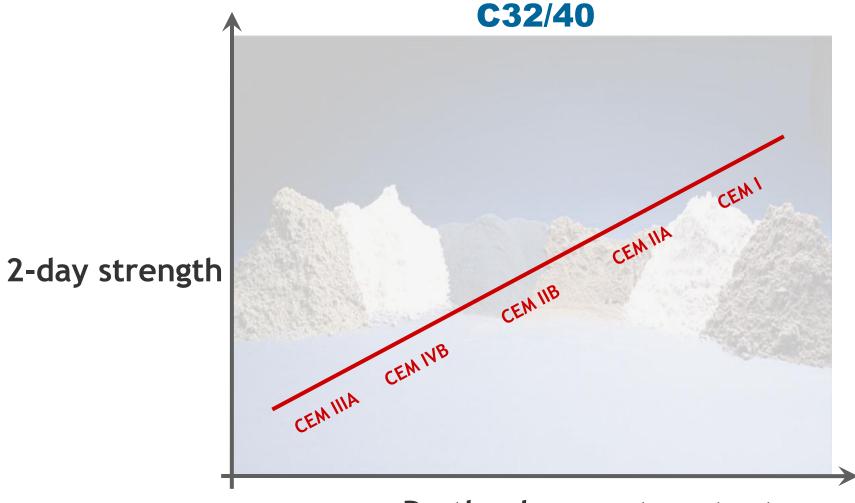




Portland cement content

Cements and combinations





Portland cement content

Portland Cement





Cement is an <u>ingredient</u> of concrete. The 'glue' that holds the mix together

Components of Ordinary Portland Cement (CEM1):

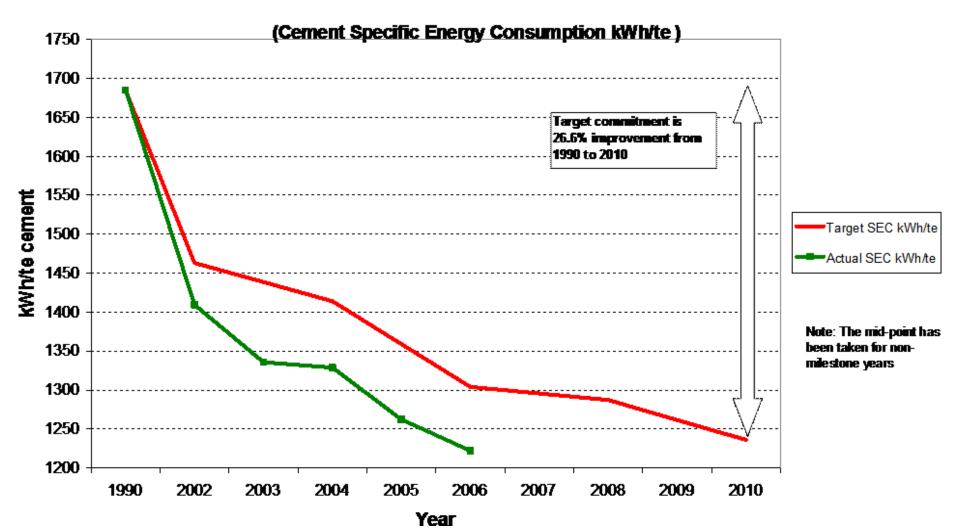
- Limestone or chalk
- Clay/Shale
- Sand
- Gypsum

Heated together at high temperature

Reduced energy use in cement production



Climate Change Agreement Performance 1990 to 2006







Material	Embodied CO ₂ (kg / tonne)	
Portland cement, CEM I		930
	Ground granulated blastfurnace slag (ggbs)	52
Addition or cement	Fly ash	4
constituent	Limestone	32
	Minor additional constituent	32
Aggregate		4
Reinforcement		427

GGBS





- Ground Granulated Blast Furnace
 Slag (GGBS) by-product from iron
- Approx 1/3 all UK ready-mixed concrete deliveries contain GGBS.
- 6-80% replacement of OPC can be used, depending on application
- lower early-age temperature rise and slower early strength gain
- Below 35-40% no impact on striking times of formwork

GGBS





- reduces eCO₂
 (50% GGBS reduces eCO₂ of concrete by 40%)
- recycled material so improves BREEAM and Green Guide rating
- inherent pale, creamy colour
- Reflectance level increased

GGBS





City of Westminster College

Schmidt Hammer Lassen / Buro Happold

• 50% GGBS - cast insitu frame

Fly Ash





- By-product from electricity generation sourced from coal fired power stations
- Used widely in block manufacture
- Improves workability and durability
- 6-55% possible depending on application
- lower early-age temperature rise and slower early strength gain
- Below 35-40% no impact on striking times of formwork

Fly Ash





- reduces ECO₂
 (30% fly ash reduces ECO₂ of concrete by 20%)
- recycled material so improves BREEAM and Green Guide rating
- inherent smokey grey colour

Other cementitious materials







Silica Fume:

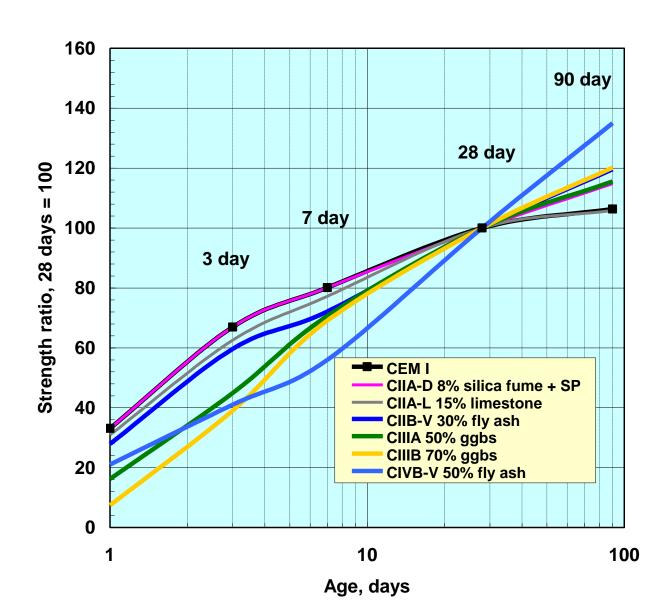
- By product of silicon manufacture
- Extremely fine powder
- Generally limited to high strength concretes or in very aggressive environmental conditions

Limestone fines:

- •To produce Portland limestone cement
- Typically limited to 6-10% replacement



Strength development





CEM III/B

(CIIIB)

Low

< CEM I

High

Longer than

CEM I

More likely

than CEM I

Less likely

than CEM I

Slow

Very good

Pozzolanic

cement

CEM IV/B-V

(CIVB-V)

Low

< CEM I

High

Longer than

CEM I

More likely than

CEM I

Less likely than

CEM I

Slow

Very good

Blastfurnace Cements

CEM III/A

(CIIIA)

Moderate

As CEM I

High

Longer than

CEM I

More likely than

CEM I

Less likely than

CEM I

Moderate

Moderate

Cem	ent type,	early	age
prop	erties		
		Cox	mont (or o

Silica fume

cement

CEM II/A-D

(CIIA-D)

High

High

High

< CEM I

Less likely

than CEM I

High

Normal/

Moderate

As CEM I

Portland

Cement

CEM I

High

Normal

Normal

Normal

Normal

Normal

Normal

Poor

Property

Early Strength

28 day Strength

Long term

Workability

Bleeding/plastic

Plastic shrinkage

Setting finishing

times

Low heat

retention

settlement

Strength

Portland

Limestone

Cement

CEM II/A-LL or L

High

As CEM I

As CEM I

Longer than

CEM I

Less likely than

CEM I

As CEM I

Normal/

Moderate

Modest

Cement type, early age		((mpa
prop	perties	The Concrete Cen
	Cement (or equivalent combination)	

Cem	ent t	type,	early	age
prop	ertie	25		
			Ceme	nt (or equ

Cem	ent type, ear	ly age	((mpa
prop	erties		The Concrete Centre

Portland fly ash

cement

CEM II/B-V

(CIIB-V)

Moderate

As CEM I

High

Longer than

CEM I

Less likely than

CEM I

As CEM I

Normal/

Moderate

Moderate

Embodied CO₂ of cements



Cement Factory made cement	Combination CEM I and addition combined at concrete plant	Secondary Main Constituent (smc) or Addition Low - High Content %	smc content Low - High, (kg CO ₂ / tonne)
CEM I Portland cement			930
CEM II/A-LL or L Portland limestone cement	CIIA-LL or L	6 - 20 limestone	880 - 750
CEM II/A-V Portland fly ash cement	CIIA-V	6 - 20 fly ash	870 - 750
CEM II/B-V Portland fly ash cement	CIIB-V	21 - 35 fly ash	730 - 610
CEM II/B-S Portland slag cement	CIIB-S	21 - 35 ggbs	740 - 620
CEM III/A Blastfurnace cement	CIIIA	36 - 65 ggbs	610 - 360
CEM III/B Blastfurnace cement	CIIIB	66 - 80 ggbs	340 - 230
CEM IV/B-V Siliceous fly ash cement	CIVB-V	36 - 55 fly ash	590 - 420

Admixtures





- Widely accepted as materials that contribute to the production of durable and cost-effective concrete structures
- Small dosages <5% by mass of cement
- Typically <1% eCO₂ of concrete
- Can assist with:
 - reducing overall eCO₂
 - reduced water use
 - extending design life of concrete



Example of use of admixtures

BS 8500 Designed concrete

Strength requirement = C32/40

- Corrosion induced by carbonation
 XC3/4 Moderate humidity or cyclic wet and dry cover = 25 + Δc mm
- From BS 8500-1: 2006 Table A.4 (50 years) then a maximum w/c of 0.55 and a minimum cement content of 260 kg/m³ is recommended.

Example of the cement content (kg/m³) C32/40 at S3 slump with a marine sand and gravel aggregate

Cement type	No admixture	Water reducing admixture (WRA)	High range water reducing admixture (HRWRA)
CEM I	315	285	250
CIIA-LL (15% limestone)	325	295	260
CIIB-V (30% fly ash)	335	300	270
CIIIA (50% ggbs)	325	295	260

Cement reduction with HRWRA

55

65

65

65

S3 slump class = 80 to 180 mm from spot samples on initial discharge

Cementitious content reduced to minimum of 260 kg/m³



This is only one example:

Other materials may well give a different pattern of results.

In particular:

The example shown is for a medium slump S3, at higher workability the use of admixtures is essential

The example shown is for rounded marine gravel with a natural sand, where other type of aggregates have a higher water demand for a given workability where the use of water reducing admixtures will be more beneficial

Responsible Sourcing



BRE Environmental & Sustainability Standard



BES 6001: ISSUE 1.0

Framework Standard for the Responsible Sourcing of Construction Products

This BRE Environmental & Sustainability Standard describes the organisational governance, supply chain management and environmental and social aspects to be addressed in the certification and approval of the responsible sourcing of construction products

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- BES 6001 is a framework standard for responsible sourcing of construction products and is the master standard against which to demonstrate compliance.
- Maximum points possible for accredited concrete products in BREEAM and The Code for Sustainable Homes.

(RSMC - Responsible Sourcing Material Credits)









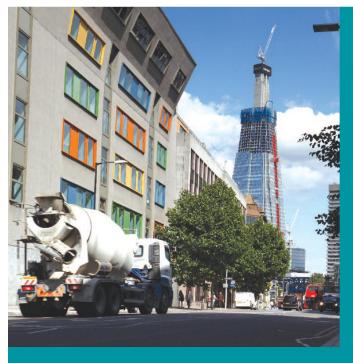












Concrete Industry Sustainability Performance Report

4th report: 2010 performance data

- 4th pan-industry sustainability report
- Measures data and sets targets over various sustainability criteria
- Industry commitment to a Sustainable Construction Strategy
- 88% surveyed concrete responsibly sourced

Further information



How to specify concrete for civil engineering structures using BS 8500

T A Harrison assumed they were not O Brooker stray, thru, note measure

Introduction

83 8300 Conceive—Complementary Shitch Translant as 65 2ht 206—11 is the medited oil specifying operate in the LNL It was remained in December 2006 principally to reflect changes made to 88E Special Regions 72 and to bring it into line with other standards.

Gadelinos are given in ISS 8500 to achieve durability of concells structures and it recommends changiful cover, manimum cameric content and manimum water/consent ratios for various appearant conditions.

This guide is intended to enable the designeer of all types of civil origineering structures to specify concrete effectively, officiently and with confidence. This guide sets out the sequeneers of BS 8500, some lightway authorities have more controls requirements that all bods be followed.

While this gaids is intended to show how to use this 9500 with favorade 2th, the advice is also generally appropriate for use with Pritich Standards however, the approach to construction obtained so given in the latter may vary from the gaidance given here.



Concrete design information

Exposure classification

Initially the relevant exposure-condition(s) should be identified in BS 8500 exposure classification is related to the deterioristics processes of calibration (XCS, regions of chlorides (RD ox XS), chemical attack from agginative gasses (ACCC) and breeze-from (XF) (see Table 1). All these deterioristics processes are sub-clinical fibre sub-districts regionary conditions; but it does not inecisionly follow that, for example, XDQ is more commons than XID. The necommendations for concrete, resistant to the XD and XS exposure classes are safficient for resistant to the exposure data. XIC The ACCC and XF exposure conditions can occur in combination with XD, XS and XC exposure classes.

Selecting concrete strength and cover

Having identified the relevant exposure condition(s), a recommended strength class and cover should be selected Table 2 (see pages and 5) indicates the normal cover and strength required to meet common superare conditions for indended vorsing lives of at least 50 or 100 years further explanation is given below. The recommendations in Table 2 are for strength, maximum maker/comment sate and minimum comment context context to reset both the primary and secondary exposures conditions statuted. The table is not strended to cover all conceive exposures straintimes and reference should be made to BS a500 for those cases not included.

Intended working life

85 8500 gives recommendations for an intended working life of at least either 50 years or 100 years. However, the Life Noboral Armer to the Eurocoder Secondmends an Indicative disagn working life of 120 years for catigory 5 structures (monamental building structures, litighway, and nativey bridges, and other cyle regimening structures). It can generally be assumed that the gardance given in \$5.9500 for at loast a 100-year working life will be appropriate for category 5 structures.

IIS 8500 notes that the recommendations for a 100-year intended working. Use in chloride conditions are subject to a degree of unertiality and consideration may be given to using barriers, coatings and comotion inhibitors, and stainless steel or non-femous reinforcement, as additional measures. Further guidance can be found in Concrete Society Technical Report 61⁸.

Compressive strength

BS 8500 uses the torm compressive straight class to define operate strength, the notation used given the cylinder trangth as well as the cube strength (see Table 3). It is important to quote the compressive strength class in full to avoid confusion.











Specifying Sustainable Concrete



Understanding the role of constituent materials

Enhancing durability



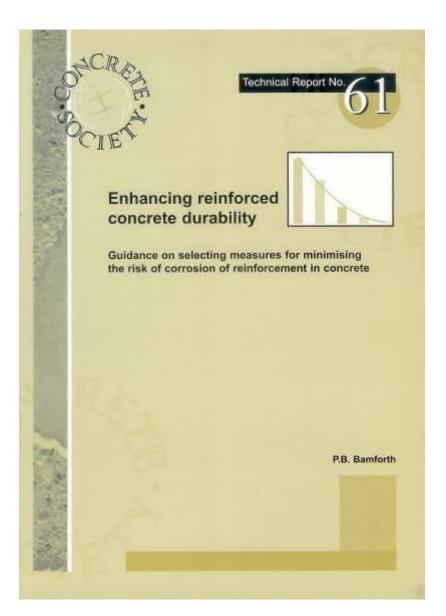
Barriers

Coatings

• Corrosion inhibitors

Stainless steel

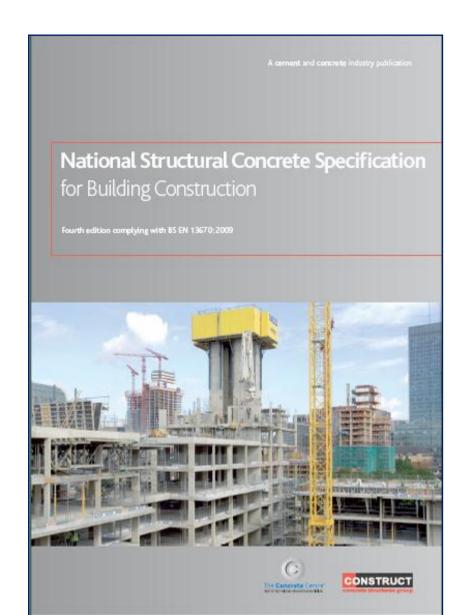
Non-ferrous rebar



NSCS 4th Edition



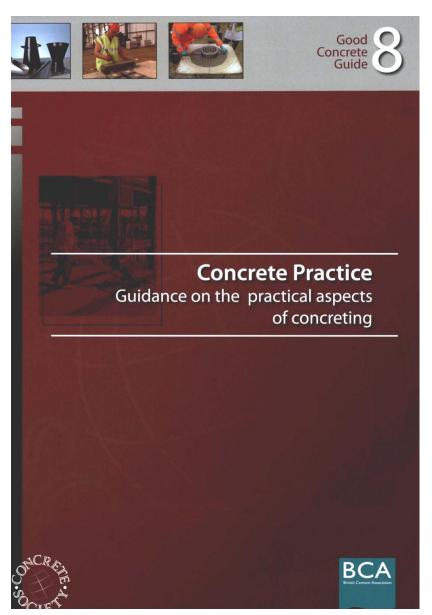
- Complies with BS EN 13670:2009
- Covers responsible sourcing clauses



Concreting

mpa
The Concrete Centre

- Transporting
- Placing and compaction
- Construction joints
- Reinforcement
- Formwork
- Curing
- Surface finishes
- Testing



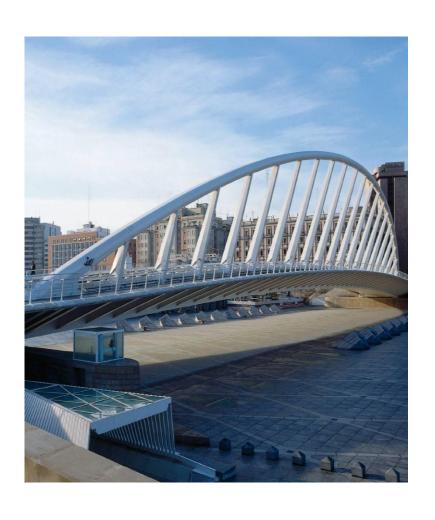


Thank you

Questions?

Specification example





Corrosion induced by carbonation (XC3/4)

Corrosion induced by chlorides (XD1)

Corrosion induced by chlorides from sea (XS3)

Freeze-thaw attack (XF4)

Chemical attack (AC-5)

Corrosion risk

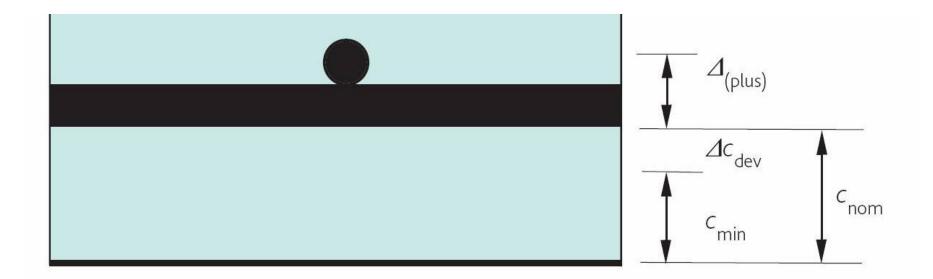


xposure con	dition	Compress			water-cement r oncrete ^c with 20				on content	Cement/Con	nbination	types
	Nominal coverb, mm	15 + Δc	$20 + \Delta c$	$25 + \Delta c$	30 + ∆c	$35 + \Delta c$	$40 + \Delta c$	45 + ∆c	50 + ∆c			
XC Ses	XC1				C20/25 0.7	0 240				All in	Table A.6	
by n, J	XC2		-		20-1	C25/30 0.65	260			All in	Table A.6	
induced by carbonation, XC exposure classes	XC3/4	-	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	S	C25/30 0	.65 260		All in Table	A.6 except	IVB
inc carbo expos	AC5/4	7-	=	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	(C25/30 0.65 26	0			IVE
sociated	XD1	7-	121	C40/50 0.45 360	C32/40 0.55 320		C28/35 0	.60 300		All in Table A.6		
ociate		is a n	(=)	·	C45/55 0.35 380	C35/45 0.45 360	(C32/40 0.50 34	0	CEM I, IIA, IIB-S, SRPC		
y as	XS1	/	-	_	C40/50 0.35 380	C32/40 0.45 360	(C28/35 0.50 34	0		IIB-V, IIIA	
for an (XC)		/	-	_	C32/40 0.40 380		C25/30 0	.50 340				IIIB, IVB
equirements are also adequate for an carbonation induced corrosion (XC)			_	-	C40/50 0.40 380	C32/40 0.50 340	(C28/35 0.55 32	0	CEM I, IIA, IIB-S, SRPC		
corr	XD2 or XS2		_	-	C35/45 0.40 380	C28/35 0.50 340	C25/30 0.55 320				IIB-V, IIIA	
e also luced		70-	-	-	C32/40 0.40, 380	C25/30 0.50, 340		020/25 0.55 32	580			IIIB, IVB
n inc		-	-	-	-	_	C45/55 0.35 380	C40/50 0.40 380	C35/45 0.45 360	CEM I, IIA, IIB-S, SRPC		
emer	XD3	/-	-	_	-	=	C35/45 0.40 380	C32/40 0.45 360	C28/35 0.50 340		IIB-V, IIIA	
carbo		3-	i - i	-	-	(C32/40 0.40 380	C28/35 0.45 360	C25/30 0.50 340			IIIB, IVB
er) K		_	_	_	-	-	_	C45/55 0.35 380	C40/50 0.40 380	CEM I, IIA, IIB-S, SRPC		
sea wat	XS3	-	<u>-</u>	-	-	-	C35/45 0.40 380	C32/40 0.45 360	C28/35 0.50 340		IIB-V, IIIA	
S		1-	12	-	-	=	C32/40 0.40 380	C28/35 0.45 360	C25/30 0.50 340			IIIB, IVB

Cover to Reinforcement



$$c_{\text{nom}} = c_{\text{min}} + \Delta c_{\text{dev}}$$



Notes

 c_{\min} = Minimum cover

 Δc_{dev} = Allowance made in design for deviation (towards face of concrete)

 $c_{\text{nom}} = c_{\text{min}} + \Delta c_{\text{dev}} = \text{nominal cover}$

Corrosion risk



xposure con	ndition	Compress	sive strength cla for no		water-cement r oncrete ^c with 20				on content	Cement/Con	nbination (types
	Nominal coverb, mm	15 + Δc	$20 + \Delta c$	$25 + \Delta c$	30 + ∆c	$35 + \Delta c$	$40 + \Delta c$	45 + ∆c	$50 + \Delta c$			
XC	XC1				C20/25 0.7	0 240				77777	Table A.6	
nduced by bonation, 2 osure class	XC2		-		30 1	C25/30 0.65	260			All in	Table A.6	
induced by carbonation, XC exposure classes	VC2/4	-	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	5:	C25/30 0	.65 260		All in Table	A.6 except	IVB
induced by carbonation, XC exposure classes	XC3/4		=	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	(C25/30 0.65 26	0			IVB
y associated	XD1	1-	=	C40/50 0.45 360	C32/40 0.55 320		C28/35 0	.60 300	3	All in	Table A.6	
sea water) Requirements are also adequate for any associated carbonation induced corrosion (XC)		15-1	(, = (,	8 - 2	C45/55 0.35 380	C35/45 0.45 360	(C32/40 0.50 34	0	CEM I, IIA, IIB-S, SRPC		
for any ass (XC)	XS1	·—	-	_	C40/50 0.35 380	C32/40 0.45 360	(228/35 0.50 34	0		IIB-V, IIIA	
for an		(-)	-	_	C32/40 0.40 380		C25/30 0	.50 340				IIIB, IVB
equirements are also adequate for an carbonation induced corrosion (XC)		-	-	-	C40/50 0.40 380	C32/40 0.50 340	(C28/35 0.55 32	0	CEM I, IIA, IIB-S, SRPC		
COLL	XD2 or XS2	_	-	-	C35/45 0.40 380	C28/35 0.50 340	(C25/30 0.55 32	0		IIB-V, IIIA	
luced		10 -1 1	-	-	C32/40 0.40, 380	C25/30 0.50, 340		020/25 0.55 32	580			IIIB, IVB
in in		-	-	-	-	_	C45/55 0.35 380	C40/50 0.40 380	C35/45 0.45 360	CEM I, IIA, IIB-S, SRPC		
enner	XD3	/ -	-	_	-	=	C35/45 0.40 380	C32/40 0.45 360	C28/35 0.50 340		IIB-V, IIIA	
equir		3-1	i - i	-	-	(C32/40 0.40 380	C28/35 0.45 360	C25/30 0.50 340			IIIB, IVB
er) K		_	_	_	-	-	_	C45/55 0.35 380	C40/50 0.40 380	CEM I, IIA, IIB-S, SRPC		
sea wate	XS3	_	<u>-</u> -	-	-	-	C35/45 0.40 380	C32/40 0.45 360	C28/35 0.50 340		IIB-V, IIIA	
Se		1-1	120	-	-	12	C32/40 0.40 380	C28/35 0.45 360	C25/30 0.50 340			IIIB, IVB

Specification example Corrosion risk



Exposure con	ndition	Compres	sive strength cla for no		water-cement r oncrete ^c with 20				inatio	n content	Cement/Con	nbination	types
	Nominal coverb, mm	$15 + \Delta c$	$20 + \Delta c$	$25 + \Delta c$	$30 + \Delta c$	$35 + \Delta c$	$40 + \Delta c$	45+	Δc	$50 + \Delta c$			
S S	XC1				C20/25 0.7	0 240					All in	Table A.6	
by by	XC2	-	_		20	C25/30 0.65	260				All in	Table A.6	
Corrosion induced by carbonation, XC exposure classes	VC2/4	-	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280		C25/30 0.0	55 260			All in Table	A.6 except	IVB
inc carbo expos	XC3/4	7-	12	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	C	25/30 0.	65 260				IVB
than d	XD1	7-1	121	C40/50 0.45 360	C32/40 0.55 320		C28/35 0.0	50 3 00		3	All in	Table A.6	
other than sociated		15-5	(= 6	8 - 2	C45/55 0.35 380	C35/45 0.45 360	С	32/40).	50 340		CEM I, IIA, IIB-S, SRPC		
XD o	XS1	/ - ·	-	_	C40/50 0.35 380	C32/40 0.45 360	C	28/35 0.	50 340			IIB-V, IIIA	
rrosion induced by chlorides (XS from sea water, XD other th sea water) Requirements are also adequate for any associated carbonation induced corrosion (XC)		ı - ı	-	_	C32/40 0.40 380		C25/30.0.	50 340					IIIB, IVB
ced by chlorides (XS from sea water lequirements are also adequate for an carbonation induced corrosion (XC)		6-1	_	-	C40/50 0.40 380	C32/40 0.50 340	С	28/35 0.	55 320		CEM I, IIA, IIB-S, SRPC		
adequ	XD2 or XS2	_	-	_	C35/45 0.40 380	C28/35 0.50 340	C	25/30 0.	55 320			IIB-V, IIIA	
e also		6 - 7	-	-	C32/40 0.40, 380	C25/30 0.50, 340	***	20/25 0.	DIOTES NO.				IIIB, IVB
nents are		_	<u></u> -	-	-	_	C45/55 0.35 380	C40/: 0.40 3	80	C35/45 0.45 360	CEM I, IIA, IIB-S, SRPC		
remer remer	XD3	7-1	-	_	-	-	C35/45 0.40 380	C31/4 0.45/3		C28/35 0.50 340		IIB-V, IIIA	
equir carbo		14-1	120	_	-	112	C	45/	55	0 10	CEM	II, II	A
er) R		-	<u>-</u>	_	-	-				0 30			
Corrosion induced sea water) Requ carl	XS3	100-00		87		_	0.3	35,	38	5 40	IIB-S	, SRI	PC
Se T			_	-	_	12	C32/40 0.40 380	C28/3	18790	C25/30 0.50 340			IIIB, IVB

Specification example Corrosion risk



Exposure con	dition	Compress			water-cement r oncrete ^c with 20				binatio	n content	Cement/Con	nbination	types
	Nominal coverb, mm	15 + Δc	$20 + \Delta c$	$25 + \Delta c$	$30 + \Delta c$	$35 + \Delta c$	$40 + \Delta c$	45 -	+ Δc	$50 + \Delta c$			
S S	XC1				C20/25 0.7	0 240					All in	Table A.6	
ass of	XC2	4-1	-		30	C25/30 0.65	260				All in	Table A.6	
induced by bonation, Joseph	VC2/4	·	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280		C25/30 0	.65 260			All in Table	A.6 except	IVB
induced by carbonation, XC exposure classes	XC3/4	7-1	121	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	(225/30	0.65 260				IVB
	XD1	1-1	124	C40/50 0.45 360	C32/40 0.55 320		C28/35 0	.60 300		3	All in	Table A.6	
AD other than 7 associated		13-51	()= 6	8 - 2	C45/55 0.35 380	C35/45 0.45 360	(C32/40	0.50 340		CEM I, IIA, IIB-S, SRPC		
ly ass	XS1	_	-	_	C40/50 0.35 380	C32/40 0.45 360	(228/35	0.50 340			IIB-V, IIIA	
sea water) Requirements are also adequate for any associated carbonation induced corrosion (XC)		·—	-	_	C32/40 0.40 380		C25/30 0	.50 340	Š				IIIB, IVB
equirements are also adequate for an		7-	-	-	C40/50 0.40 380	C32/40 0.50 340	(28/35	0.55 320		CEM I, IIA, IIB-S, SRPC		
corr	XD2 or XS2	_	-	-	C35/45 0.40 380	C28/35 0.50 340	(225/30	0.55 320			IIB-V, IIIA	
nents are also ation induced			-	-	C32/40 0.40, 380	C25/30 0.50, 340		000000000000000000000000000000000000000	0.55 320	W			IIIB, IVB
nts ar		_	-	-	-	_	C45/55 0.35 380	0.40		C35/45 0.45 360	CEM I, IIA, IIB-S, SRPC		
emer	XD3	/ -	-	-	-	-	C35/45 0.40 380	0.45		C28/35 0.50 340		IIB-V, IIIA	
equirer		1-	12	<u>- (1</u>)	P=0	18	C32/40 0.40 380	C2: 0.4.	360 360	C25/30 0.50 340			IIIB, IVB
er) R		_	_	-	-	-	C	32	/40	0 30	III	B-V	
ı wat	XS3		N=41	10 10 10 10 10 10 10 10 10 10 10 10 10 1	-	-				5			
sea water) Requ		-	120	-	-		0.4	45 ,	36	0		IIA	

Specification example Corrosion risk



Exposure con	dition	Compress			water-cement r oncrete ^c with 20	atio and minim) mm maximun			binatio	n content	Cement/Con	nbination	types
	Nominal coverb, mm	15 + ∆c	$20 + \Delta c$	$25 + \Delta c$	$30 + \Delta c$	$35 + \Delta c$	$40 + \Delta c$	45+	Δc	$50 + \Delta c$			
KC ses	XC1				C20/25 0.7	0 240					All in	Table A.6	
on by by	XC2	1-1	(- 8		20-1	C25/30 0.65	260				All in	Table A.6	
Corrosion induced by bonation, ?	XC3/4	_	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	\$	C25/30 0.	.65 260			All in Table	A.6 except	IVB
Corrosion induced by carbonation, XC exposure classes	AC3/4	1-1	_	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	C	25/30	.65 260				IVB
an	XD1	1-1	121	C40/50 0.45 360	C32/40 0.55 320		C28/35 0.	.60 300		3	All in	Table A.6	
other than sociated		12-12	(= 6	-	C45/55 0.35 380	C35/45 0.45 360	C	32/40	.50 340		CEM I, IIA, IIB-S, SRPC		
XD o	XS1	(-	-	_	C40/50 0.35 380	C32/40 0.45 360	C	228/35	.50 340			IIB-V, IIIA	
water, for an (XC)		-	-	_	C32/40 0.40 380		C25/30.0	.50 340					IIIB, IVB
ced by chlorides (XS from sea water sequirements are also adequate for an carbonation induced corrosion (XC)		15 -	_	-	C40/50 0.40 380	C32/40 0.50 340	C	228/35).55 320		CEM I, IIA, IIB-S, SRPC		
fron	XD2 or XS2	_	_	-	C35/45 0.40 380	C28/35 0.50 340	C	25/30).55 320			IIB-V, IIIA	
e also		· -	_	-	C32/40 0.40, 380	C25/30 0.50, 340		2007/2019/2019).55 320				IIIB, IVB
chlorides nemts are ation indu			<u></u> -	-		_	C45/55 0.35 380	C40 0.40	380	C35/45 0.45 360	CEM I, IIA, IIB-S, SRPC		
oy cu iremet	XD3	/ 	-	-	-	=	C35/45 0.40 380	C32 0.45	360	C28/35 0.50 340		IIB-V, IIIA	
ced requir		7-1		12.0	(* <u></u>):	150	C32/40 0.40 380	C28 0.45		C25/30 0.50 340			IIIB, IVB
in C R			-	_	-	_	-	C4: 0.3		C40/50 0.40 380	CEM I, IIA, IIB-S, SRPC		
Corrosion sea wate	XS3	- 100 M			_	_	C	28	/35	5		IIB	
Corr		-	(=)	_	-	=	(0			

Corrosion risk



xposure con	ndition	Compres	sive strength cla for no			atio and minim mm maximun			on content	Cement/Cor	nbination	ypes
	Nominal coverb, mm	15 + Δc	$20 + \Delta c$	$25 + \Delta c$	$30 + \Delta c$	$35 + \Delta c$	$40 + \Delta c$	$45 + \Delta c$	$50 + \Delta c$			
XC	XC1				C20/25 0.7	70 240		*		All in	Table A.6	
on by	XC2		-		20	C25/30 0.65	260			All in	Table A.6	
Corrosion induced by carbonation, XC exposure classes	VC2/4		C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280		C25/30 0	.65 260		All in Table	A.6 except	IVB
inc carbo expos	XC3/4	7-	1=1	C40/50 0.45 340	C32/40 0.55 300	C28/35 0.60 280	,	C25/30 0.65 26	0			IVB
water, XD other than for any associated (XC)	XD1	1-	(=)	C40/50 0.45 360	C32/40 0.55 320		C28/35 0	.60 300		All in	Table A.6	
ociate		1955	(= 5)	,—,	C45/55 0.35 380	C35/45 0.45 360		C32/40 0.50 34	0	CEM I, IIA, IIB-S, SRPC		
y ass	XS1	-	-	_	C40/50 0.35 380	C32/40 0.45 360	1	C28/35 0.50 34	0		IIB-V. IIIA	
rrosion induced by chlorides (XS from sea water, XD other th sea water) Requirements are also adequate for any associated carbonation induced corrosion (XC)		_	-	_	C32/40 0.40 380		C25/30 ().50 340				IIIB, IVB
(XS from sea also adequate ced corrosion		75-	_	-	C40/50 0.40 380	C32/40 0.50 340		C28/35 0.55 32	0	CEM I, IIA, IIB-S, SRPC		
aded	XD2 or XS2		_	-	C35/45 0.40 380	C28/35 0.50 340	49	C25/30 0.55 32	0		IIB-V, IIIA	
rements are also onation induced		16 -1 1	_	-	C32/40 0.40, 380	C25/30 0.50, 340		C20/25 0.55 32	200			IIIB, IVB
nts ar		·	-	-	-	_	C45/55 0.35 380	C40/50 0.40 380	C35/45 0.45 360	CEM I, IIA, IIB-S, SRPC		
emer	XD3	(-	-	-	_	=	C35/45 0.40 380	C32/40 0.45 360	C23/35 0.50 340		IIB-V, IIIA	
equin		==	- :	<u>(ii)</u>	-	120	C32/40 0.40 380	C28/35	C2 30			IIIB,
er) Requ		-	-	-	-	-	-	C28/3	35	CEM IIB-S,	IB-V	
sea wate	XS3						C35/45 0.40 38			-		
se			=	-	-	-	C32/40 0.40 38	0.50,	340		IIIA	



Exposure				Re	quireme	nts for desi	gned concretes					
class	Minimum strength class	Maximu m w/c ratio	cemer	t or com	bination	inimum content regate size	Other requirements	Cements and combinations				
	Class		32 mm or 40 mm	20 mm	14 mm	10 mm						
	C25/30	0.60	3.0	3.5	4.5	5.5	90.00					
	LC25/28		260	280	300	320						
XF1	C28/35	0.60	_	_	-	_	-					
	LC28/31		260	280	300	320		- All in Table A.6				
	C25/30	0.60	3.0	3.5	4.5	5.5		All in Table A.6				
	LC25/28		260	280	300	320						
XF2	C32/40	0.55	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-	(-	Section 1	†				
	LC32/35		280	300	320	340						
	C25/30	0.60	3.0	3.5	4.5	5.5		All in Table A.6				
XF3	LC25/28		260	280	300	320						
AFS	C40/50	0.45	(<u>===</u>	200	<u></u>	2	7:	excluding cement and combination type IVB				
	LC40/44		320	340	360	360	Freeze/thaw	combination type IVB				
	C28/35	0.55	3.0	3.5	4.5	5.5	resisting	PHILIPPOP (12) I TREED INVOICED TO THE TOOLS				
XF4	LC28/31	10000000000000000000000000000000000000	280	300	320	340	aggregates ^b	Alle in Table A.6 excluding cement and				
	C40/50	0.45	(4-4)	<u> </u>	6 91	944-77	1	combination type IVB				
	LC40/44		320	340	360	360		(A)				



Exposure class				Re	quireme	nts for desi	gned concretes				
Class	Minimum strength class	Maximu m w/c ratio	cemen	t or com	bination	inimum content regate size	Other requirements	Cements and combinations			
	CM35		32 mm or 40 mm	20 mm	14 mm	10 mm					
	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5	5.5 320	<u> </u>				
XF1	C28/35	0.60		_			_				
	LC28/31		260	280	300	320					
	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320	_	All in Table A.6			
XF2	C32/40 LC32/35	0.55		300	320	340	_				
3700	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320		All in Table A.6			
XF3	C40/50 LC40/44	0.45	320	340	360	360	Freeze/thaw resisting aggregatesb	excluding cement and combination type IVB			
XF4	C28/35 LC28/31	0.55	3.0 280	3.5 300	4.5 320	5.5 340		Alle in Table A.6			
and the state of t	C40/50 LC40/44	0.45	320	340	360	360	-	excluding cement and combination type IVB			



Exposure				Re	quireme	nts for desi	gned concretes	
class	Minimum strength class	Maximu m w/c ratio	cemen	tor com	bination	inimum content regate size	Other requirements	Cements and combinations
	Causs		32 mm or 40 mm	20 mm	14 mm	10 mm		
-110	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320	<u> </u>	
XF1	C28/35 LC28/31	0.60		280	300	320		
	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320		All in Table A.6
XF2	C32/40 LC32/35	0.55		300	320	340	_	
XF3	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320		All in Table A.6 excluding cement and
AFS	C40/50 LC40/44	0.45	320	34	 360	360	Freeze/thaw	combination type IVB
XF4	C 2	28/35,	0.55	, 30	0, 3.	.5	resisting aggregates ^b	All (except IVB
	C40/50 LC40/44	0.45	320	340	360	360		combination type IVB



Exposure class				Re	quireme	nts for desi	gned concretes				
Ciuss	Minimum strength class	Maximu m w/c ratio	cemen	tor com	it ^a and m bination num agg		Other requirements	Cements and combinations			
	Class		32 mm or 40 mm	20 mm	14 mm	10 mm					
	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320	<u> </u>				
XF1	C28/35 LC28/31	0.60		280	300	320					
	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320	_	All in Table A.6			
XF2	C32/40 LC32/35	0.55		300	320		_				
XF3	C25/30 LC25/28	0.60	3.0 260	3.5 280	4.5 300	5.5 320		All in Table A.6 excluding cement and			
AFS	C40/50 LC40/44	0.45	320	340	360	360	Freeze/thaw	combination type IVB			
XF4	C28/35 LC28/31	0.55	3.0 280	3.5	4.5 320	5.5 340	resisting aggregates ^b	Allc in Table A.6			
		C40/5	60, O.	45,	340			All (except IVB			



ACEC Class	Lowest	Inten	ded working life
	nominal cover ^{e, f} , mm	At least 50 years g, h	At least 100 years
AC-1s, AC-1	$(25 + \Delta c)$	DC-1 (RC25/30 if reinforced)	DC-1 (RC25/30 if reinforced)
AC-2s, AC-2	$(25 + \Delta c)$	DC-2 (FND2)	DC-2 (FND2)
AC-2z	$(25 + \Delta c)$	DC-2z (FND2z)	DC-2z (FND2z)
AC-3s	$(25 + \Delta c)$	DC-3 (FND3)	DC-3 (FND3)
AC-3z	$(25 + \Delta c)$	DC-3z (FND3z)	DC-3z (FND3z)
AC-3	$(25 + \Delta c)$	DC-3 (FND3)	DC-3 + one APM of choice, FND3 + one APM of choice, DC-4 or FND4
AC-4s	$(25 + \Delta c)$	DC-4 (FND4)	DC-4 (FND4)
AC-4z	$(25 + \Delta c)$	DC-4z (FND4z)	DC-4z (FND4z)
AC-4	$(25 + \Delta c)$	DC-4 (FND4)	DC-4 + one APM from APM2 to APM5, or FND4 + one APM from APM2 to APM5
AC-4ms	$(25 + \Delta c)$	DC-4m (FND4m)	DC-4m (FND4m)
AC-4m	$(25 + \Delta c)$	DC-4m (FND4m)	DC-4m + one APM from APM2 to APM5, or FND4m + one APM from APM2 to APM5
AC-JZ	$(25 + \Delta c)$	DC-4z (FND4z) + APM3i	
AC-5	$(25 + \Delta c)$	DC-4 (FND4) + APM3i	DC-4 (+ APM3)
AC-5m	$(25 + \Delta c)$	DC-4m (FND4m)+ APM3 ⁱ	DC-+III (LIAD+III) + VLIAI2.



DC-class	Maximum w/c ratio		content ir naximum	nt or com n kg/m³ fo n aggrega mm) of:	or	Cement and combination types
		≥ 40	20	14	10	
DC-1 ^a	s s	-	-		-	All in Table A.6
	0.55	300	320	340	360	IIB-V+SR, IIIA+SR, IIIB+SR, IVB
DC 2	0.50	320	340	360	380	CEM I, SRPC, IIA-D, IIA-Q, II-S, II-V,
DC-2				,	(IIIA, IIIB
	0.45	340	360	380	380	IIA-L or LL \geq 42,5
	0.40	360	380	380	380	IIA-L or LL 32,5
DC-2z	0.55	300	320	340	360	All in Table A.6
sees and order	0.50	320	340	360	380	IIIB+SR
DC-3	0.45	340	360	380	380	IVB
	0.40	360	380	380	380	IIB-V+SR, IIIA+SR, SRPC
DC-3z	0.50	320	340	360	380	All in Table A.6
page 1 (1966) - 96	0.45	340	360	380	380	IIIB+SR
DC-4	0.40	360	380	380	380	IVB
	0.35	380	380	380	380	IIB-V+SR, IIIA+SR, SRPC
DC-4z	0.45	340	360	380	380	All in Table A.6
DC-4m	0.45	340	360	380	380	IIIB+SR



DC-class	Maximum w/c ratio	Minimum cement or combination content in kg/m ³ for maximum aggregate sizes (mm) of:				Cement and combination types	
D.C.		≥ 40	20	14	10		
DC-1a	-	8			-	All in Table A.6	
	0.55	300	320	340	360	IIB-V+SR, IIIA+SR, IIIB+SR, IVB	
DC-2	0.50	320	340	360	380	CEM I, SRPC, IIA-D, IIA-Q, II-S, II-V, IIIA, IIIB	
	0.45	340	360	380	380	IIA-L or LL \geq 42,5	
	0.40	360	380	380	380	IIA-L or LL 32,5	
DC-2z	0.55	300	320	340	360	All in Table A.6	
ma saisealt	0.50	320	340	360	380	IIIB+SR	
DC-3	0.45	340	360	380	380	IVB	
	0.40	360	380	380	380	IIB-V+SR, IIIA+SR, SRPC	
DC-3z	0.50	320		360	380	A.6	
500 000 70	0.45	340 ▶	360	- 380	380	IIIB+SR	
DC-4		360		380	380	1110	
	0.35	380	380	380	380	IIB-V+SR, IIIA+SR, SRPC	
DC-4z	0.45	340	360	380	380	All in Table A.6	
DC-4m	0.45	340	360	380	380	IIIB+SR	



DC-class	Maximum w/c ratio	Minimum cement or combination content in kg/m³ for maximum aggregate sizes (mm) of:				Cement and combination types		
D.C. 1.		≥ 4 0	20	14	10			
DC-1a		S		*	-	All in Table A.6		
	0.55	300	320	340	360	IIB-V+SR, IIIA+SR, IIIB+SR, IVB		
DC-2	0.50	320	340	360	380	CEM I, SRPC, IIA-D, IIA-Q, II-S, II-V,		
DC-2	87			Y .	(IIIA, IIIB		
	0.45	340	360	380	380	IIA-L or $LL \ge 42,5$		
	0.40	360	380	380	380	IIA-L or LL 32,5		
DC-2z	0.55	300	320	340	360	All in Table A.6		
soc netroils	0.50	320	340	360	380	IIIB+SR		
DC-3	0.45	340	360	380	380	IVB		
	0.40	360	380	380	380	IIB-V+SR, IIIA+SR, SRPC		
DC-3z	0.50	320	340	360	380	All in Table A.6		
500 005 00	0.45	340	200	380	380			
DC-4	0.40	360 ▶	380	380	380	IVB		
	20 STATE PARTIE	380	500	380	380	III VISIK, AIIA+SR, SRPC		
DC-4z	0.45	340	360	380	380	All in Table A.6		
DC-4m	0.45	340	360	380	380	IIIB+SR		



DC-class	Maximum w/c ratio	Minimum cement or combination content in kg/m ³ for maximum aggregate sizes (mm) of:				Cement and combination types		
501		≥ 40	20	14	10			
DC-1 ^a					-	All in Table A.6		
	0.55	300	320	340	360	IIB-V+SR, IIIA+SR, IIIB+SR, IVB		
DC-2	0.50	320	340	360	380	CEM I, SRPC, IIA-D, IIA-Q, II-S, II-V, IIIA, IIIB		
	0.45	340	360	380	380	IIA-L or LL \geq 42,5		
	0.40	360	380	380	380	IIA-L or LL 32,5		
DC-2z	0.55	300	320	340	360	All in Table A.6		
sau saire di	0.50	320	340	360	380	IIIB+SR		
DC-3	0.45	340	360	380	380	IVB		
	0.40	360	380	380	380	IIB-V+SR, IIIA+SR, SRPC		
DC-3z	0.50	320	340	360	380	All in Table A.6		
500 005 00	0.45	340	360	380	380	IIIB+SR		
DC-4	0.10	360		380	380			
	0.35	380	380	380	380	IIB-V+SR, IIIA+SR, SRPC		
DC-4z		340	200	380	380	All III Table A.o		
DC-4m	0.45	340	360	380	380	IIIB+SR		



Table A.10 — Additional protective measures (APMs)					
Option code	APM				
APM1	Enhanced concrete quality				
APM2	Use of controlled permeability formwork				
APM3	Provide surface protection				
APM4	Provide sacrificial layer				
APM5	Address drainage of site				

Example specification



Exposure class	Strength class	Maximum W/C ratio	Minimum cement content (kg/m³)	Air content (%)	Allowable cements
	C45/55	0.35	380		CEMI, IIA, IIB-S
X3S	C32/40	0.45	360	~	IIB-V, IIIA
	C28/35	0.45	360		IIIB, IVB
VEA	C28/35	0.55	300	3.5	All (2002204 IVD)
XF4	C40/50	0.45	340	~	All (except IVB)
		0.45	360	~	IIIB + SR
DC-4	~	0.35	380		IVB
		0.30	380		IIB + SR; IIIA + SR

Example specification



Option A

Exposure class	Strength class	Maximum W/C ratio	Minimum cement content (kg/m³)	Air content (%)	Allowable cements
	C45/55	0.35	380		CEMI, IIA, IIB-S
X3S	C32/40	0.45	360	~	IIB-V, IIIA
	C28/35	0.45	360		IIIB, IVB
VEA	C28/35	0.55	300	3.5	All (except IVP)
XF4	C40/50	0.45	340	~	All (except IVB)
		0.45	360		IIIB + SR
DC-4	~	0.35	380	~	IVB
		0.30	380		IIB + SR; IIIA + SR

Example specification



Option B

Exposure class	Strength class	Maximum W/C ratio	Minimum cement content (kg/m³)	Air content (%)	Allowable cements
	C45/55	0.35	380		CEMI, IIA, IIB-S
X3S	C32/40	0.45	360	~	IIB-V, IIIA
	C28/35	0.45	360		IIIB, IVB
XF4	C28/35	0.55	300	3.5	All (except IVB)
ΛΓ4	C40/50	0.45	340	~	
	~	0.45	360	~	IIIB + SR
DC-4		0.35	380		IVB
		0.30	380		IIB + SR; IIIA + SR



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